

## Adsorption of Iron (II) Ions from Aqueous Solution using Activated Carbon from *Averva lanata*

C. Jayajothi, M. M. Senthamilselvi, M. Ajithkumar, S. Arivoli

Received 2 June 2022, Accepted 11 August 2022, Published 19 October 2022

### ABSTRACT

*Averva lanata* obtained from nearby Poompuhar, having the high surface area was used as an adsorbent for the removal of Fe (II) ion from aqueous solution. The effect of various factors (temperature, adsorbent dose and Initial pH) on adsorption of Fe (II) on *Averva lanata* was investigated. The effect of pH shows that the amount adsorbed increased with the increase of pH of solution. The equilibrium adsorption isotherms were analyzed by Langmuir and Freundlich equations. Both Langmuir and Freundlich models can describe the adsorption equilibrium but the Langmuir model shows better agreement. The amount adsorbed increased with the increase of temperature suggests the formation of dimer in the contact region. SEM

micrographs and differential molar isosteric heat of adsorption ( $\Delta H$ ) calculated at different surface coverage, indicate that the surface is heterogeneous having energetically different adsorption sites. Values of  $n$  calculated from Freundlich plots indicate that adsorption of Fe (II) on *Averva lanata* is spontaneous. At high surface coverage, the differential heat of adsorption versus surface coverage plot shows maximum value indicating the occurrence of structural rearrangement in the adsorbate. With the increase of adsorbent dose, amount adsorbed increased due to the increased surface area of adsorbent.

**Keywords** Iron, Activated *Averva lanata* carbon (AALC), Adsorption models, Equilibrium.

### INTRODUCTION

Water is the main component for living organisms, and the increase in water pollution as a result of progress in the industrial technologies, has been reduced using many methods to treat the wastewater (Chapman 1992). The choice of suitable methods is controlled by different factors such as the efficiency of removing the pollutant materials, the availability of the used chemicals and the chemistry of the contaminated materials beside the process cost (Letterman 1999). It is well-known that the pollutants in wastewater discharge from industrial effluents, sewage,

---

C. Jayajothi  
Research Scholar, Periyar E.V. R. College, Affiliated to Bharathidasan University, Thiruchirappalli

M. M. Senthamilselvi  
Principal (Retd), Kamarajar Government Arts College Surandai, Thirunelveli, Tamilnadu, India

M. Ajithkumar, S. Arivoli\*  
Principal, Poompuhar College (Autonomous), Affiliated to Bharathidasan University, Melaiyur 620024, Tamilnadu, India  
Email : arivu6363@gmail.com

\*Corresponding author

sludge, pesticides, and fertilizers. The composition of the contaminated water depends on the source of the pollutant, the chemical composition of the original water whether it is surface or underground water and then the chemical reaction with the soil. For example, groundwater contains one or more contaminants like iron, manganese, ammonium, methane and natural organic matter, e.g., humic acid. Hence, before using this water supply for agro-irrigation purposes, these contaminants should be removed or reduced to the acceptable levels. Iron and manganese, which are usually present in the groundwater as divalent cations, considered to be contaminants mainly due to their organoleptic properties. The maximum recommended levels of Fe in drinking water are 0.3 mg/L, respectively. There are various methods for removing Fe (II) cations from the wastewater including ion-exchange method (Vaaramaa 2003), oxidation by oxidizing agents such as chlorine and potassium permanganate (Ellis 2000), activated carbon and/or other filtering materials, supercritical fluid extraction, bioremediation and treatment with limestone (Bin Jusoh 2005). Some of these methods are simple and economic while the others are complicated and expensive. In oxidation treatment, oxygen, chlorine or potassium permanganate ( $\text{KMnO}_4$ ), is generally used for Fe (II) oxidation. Adsorption using activated carbon is an effective technique to remove heavy metals from wastewater that is due to that activated carbon has pore size distributions which control its adsorption capacity, a chemical structure that influences its interaction with polar and non-polar adsorbate, and active sites which determine the type of chemical reactions with other molecules (Munter 2005).

However, in developing countries such as India, traditional activated carbon remains an expensive material for heavy metal removal. Recently, many researchers have been published in the literature including preparation of activated carbons from various cheaper and alternative materials, e.g., agricultural by-products and biomass materials, using chemical activation with  $\text{H}_3\text{PO}_4$  (Okoniewska 2007). However, there is only limited research on the preparation of activated carbons from woody biomass such as sawdust for uptaking heavy metals such as Hg (II) from wastewaters reported that the removal of Fe, Mn and Cu ions from acid mine drainage (AMD) by precipitation with NaOH depends on the pH value besides the

oxidation state of the removed cations. On the other hand, various authors found that the removal of iron and other heavy metals by activated carbon depends on the nature of carbon (porosity, surface area, oxygen functional groups). Within the frame of this policy, the present paper narrates the investigation of Fe (II) ions removal from aqueous solution using adsorption methods in order to determine the optimum pH for the effective removal (Berbenni 2000). The adsorption was carried out using an activated carbon obtained from *Averva lanata*. The adsorption data was analyzed by using Langmuir and Freundlich isotherm models. Overall, this study was also intended to determine the efficiency and the optimum conditions in adsorption processes for removal of iron cations.

## MATERIALS AND METHODS

### Adsorbent

The natural plant material *Averva lanata*, used in the present investigations was collected from agricultural area the stems were washed with distilled water several times to remove the dirt and dust and was subsequently dried in a hot air oven at  $110^\circ\text{C}$ . Afterward, carbonization of the *Averva lanata* was activated at  $600^\circ\text{C}$  for 1 h in a muffle furnace. The activated carbon was thereafter looked to room temperature in an insert atmosphere of nitrogen and washed with hot distilled water and 0.5 N Hydrochloric and until the pH of the material reached 7.0 the activated carbon was also dried in a hot air oven at  $110^\circ\text{C}$ , ground, sieved and stored in desiccators for further use.

### Chemicals

All chemicals used of high purity commercially available Analar grade purchased from scientific equipment company trichy. Iron solution was prepared from  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$  (2.489 g in 500 ml distilled water equivalent to one gram/liter). All experimental solutions were prepared by diluting the stock solution to the required concentration. The pH of each experimental solution was adjusted to the required initial pH value using dilute HCl (or) NaOH before mixing the adsorbent. The concentration of residual Iron (II) was determined with atomic absorption spectrophotometer (Perkin Elemer 2380).

### Batch experiments

The effect of various parameters on the removal of Iron (II) onto AALC was studied batch adsorption experiments were conducted at (30-60°C). For each experimental run, 50 ml of iron solution of known initial concentration and pH were taken in a 250 ml plugged conical flask. A 25 mg adsorbent dose is added to the solution and mixture was shaken at constant agitation speed (200 rpm) sample were withdrawn at appropriate time intervals (10-60 min) and the adsorbent was separated by filtration (Aziz 2004). The residual solutions were analyzed to determine the Iron (II) concentration.

The effect of dosage of adsorbent on the removal of Iron (II) was measured by contacting 50 ml of 50 mg/L of Iron (II) solution with 25 mg of AALC till equilibrium was attained.

Adsorption equilibrium isotherm is studied using 25 mg of AALC dosage per 50 ml of Iron (II) solution. The initial concentration were ranged from (25 to 125 mg/L) in all sets of experiments. The plugged conical flask was shaken at a speed of 200 rpm for 60 minutes. Then the solution was separated from the mixture and analyzed for Iron (II) concentration (Ahmedna 2004). The adsorption capacity was calculated by using a mass equilibrium equation as follows:

$$q_e = (C_0 - C_e) V/M \dots\dots\dots (1)$$

Where  $C_0$  and  $C_e$  being the initial iron concentration (mg/L) and equilibrium concentration, respectively  $V$  is the experimental volume of Iron (II) solution expressed in liters [L] and  $M$  is the adsorbent mass expressed in grams [g]. The Iron (II) ions percentage can be calculated as follows:

$$\% R = (C_0 - C_t) \times 100/C_0 \dots\dots\dots (2)$$

The effect of pH on the rate of adsorption was investigated using iron concentration of 25 mg/L constant AALC dosage. The pH values were adjusted with dilute HCl and NaOH solution. The adsorbent – adsorbate mixture was shaken at room temperature using agitation speed (200 rpm) for 60 minutes. Then the concentration of Iron in solution was determined.

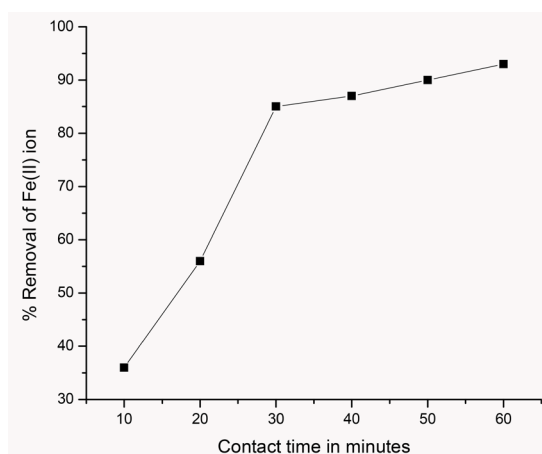
## RESULTS AND DISCUSSION

### Adsorption studies

Batch experiments were performed to investigate the adsorption process of Fe (II) by the AALC. For each experimental run, 50 mL of Fe (II) solution of known concentration, initial pH, ionic strength and the amount of the AALC were taken in a 250-mL stoppered conical flask (El-Sherif 2011). This mixture was agitated in a temperature-controlled shaking water bath at a constant speed of 200 rpm/min and certain temperatures. For adsorption equilibrium studies, Fe (II) solutions of different concentrations were contacted with a certain amount of AALC under certain conditions for an hr insuring the equilibrium was achieved. The residual Fe (II) concentration was then measured and the amount of Fe (II) adsorbed onto AALC was calculated from mass balance. Effects of contact time, adsorbent dosage, initial Fe (II) concentration, initial solution pH on Fe (II) adsorption by AALC were investigated. Adsorption kinetics was determined by analyzing adsorptive uptake of Fe (II) from aqueous solution at different time intervals. The amount of Fe (II) adsorbed at time  $t$ ,  $q_t$  (mg/g), was calculated using mass balance equation and the equilibrium data given in Table 1 (Girgis 2007).

**Table 1.** Equilibrium parameters for the adsorption of Iron (II) ion onto AALC

$M_0$	Ce (Mg / L)				Qe (Mg / L)				Removal %			
	30°C	40°C	50°C	60°C	30°C	40°C	50°C	60°C	30°C	40°C	50°C	60°C
25	3.74	3.13	2.64	2.13	92.70	93.92	94.90	94.52	92.72	93.92	94.90	94.52
50	11.93	10.56	8.48	7.66	177.1	179.0	183.0	184.8	88.56	89.53	91.52	92.43
75	25.94	22.36	19.64	17.36	248.5	255.2	260.7	265.2	82.83	85.08	86.90	88.42
100	47.84	43.64	19.64	36.67	304.3	312.7	360.7	326.6	76.07	78.17	90.17	81.66
125	73.88	69.93	40.64	60.90	352.2	360.1	418.7	378.19	70.44	72.02	83.74	75.63



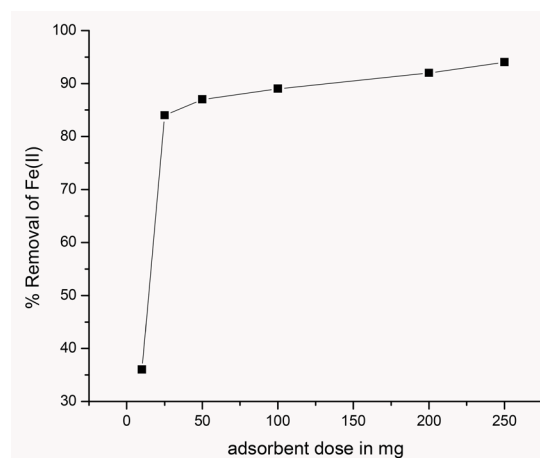
**Fig. 1.** Effect of contact time on the removal of Fe (II) ion [Fe (II)]=50 mg/L; Temperature 30°C; Adsorbent dose = 0.025 g /50 m L.

#### Effect of contact time on batch Adsorption of Iron (II) ions in Aqueous Solution

Fig.1. shows the effect of contact time on the adsorption of Iron (II) ions solution using activated carbon from *Averva lanata*. The concentrations of iron (II) ions in solution were varied from 25 mg/L to 125 mg/L and batch adsorption was carried out with 25 mg of activated *Averva lanata* carbon. The percentage of iron (II) ions adsorbed increased with time until equilibrium was reached for each concentration. It is therefore evident from Fig.1, that at low concentration ranges the percent adsorption is high because of the availability of more reactive sites. At higher concentration of metal ion more and more surface sites are covered, the capacity of the adsorbent get exhausted due to non-availability of active surface sites. This leads to a fall in the percentage of metal ion adsorbed at higher concentration. It was observed that the percentage adsorption of iron (II) ion rapidly reached equilibrium at 30 minutes of contact for 25 mg/L concentration, it increased to 100% implied that iron (II) ( $\text{Fe}^{2+}$ ) ion was completely removed from aqueous solution at this concentration (Kazemipour 2008).

#### Effect of initial concentration on the adsorption of Iron (II) ion in aqueous solution

The effect of initial concentration of iron (II) ions

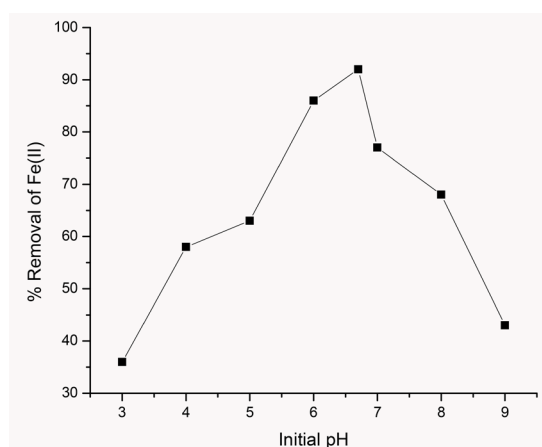


**Fig. 2.** Effect of adsorbent dose on the removal of Fe (II) ion [Fe (II)]=50 mg/L; Temperature 300C; contact time 60 min.

on adsorption of iron (II) ions using *Averva lanata* activated carbon. Adsorption of iron (II) ions in solution increase significantly with reduction in the initial concentration of iron (II) ions in solution. The initial concentration of adsorbate varied from 25 mg/L to 125 mg/L. The rate of adsorption decreased as the concentration of iron (II) ions increased from 25 mg/L to 125 mg/L within 30 min of adsorption. This was expected and shows that there more reactive sites on the *Averva lanata* activated carbon (Balintova 2010).

#### Effect of Carbon Dosage on the Batch Adsorption of Iron (II) Ions in Aqueous Solution

Iron (II) ions in aqueous solution of known concentration was adsorbed using different carbon dosage of activated *Averva lanata* ranging from 25 mg – 125 mg in 50 ml of stock solution of iron (II) ions . The effect of carbon dosage on the adsorption of iron (II) ions using activated carbon from waste *Averva lanata* is presented in Fig. 2. There was significant increase in the adsorption of iron (II) ions in solution as carbon dosage increased within adsorption time of 30 min reported similar findings during the removal of heavy metal adsorption by modified oak sawdust. This is due to the increased availability of active adsorption sites arising due to the increase in effective surface area resulting from the increases in dose of adsorbent or due to conglomeration of the adsorbent. Increasing



**Fig. 3.** Effect of initial pH on the removal of Fe (II) ion [Fe(II)]=50 mg/L; Temperature 30°C; Adsorbent dose=0.025 g/ 50 mL.

the adsorbent dosage further, it was found that the optimum uptake of iron (II) ions requires about 250 mg of activated carbon from *Averva lanata* to adsorb 100% iron (II) ions in aqueous stock iron (II) solution (Hamadi 2004).

#### Effect of particle size on the batch adsorption of Iron (II) ions in aqueous solution

Effect of particle size of activated carbon produced from waste *Averva lanata* the batch adsorption of iron (II) ions in aqueous solution. The adsorption of iron (II) ions increased with reduction in particle size (Sharma and Bhattacharya 2005). The shape reduction also revealed that particle size of activated *Averva lanata* carbon has significant effect on the adsorption of iron (II) ions in aqueous solution for batch process. Smaller particle size dsorbed the highest amount of

**Table 2.** Langmuir and Freundlich Isotherm Parameters for the adsorption of Iron (II) ion Onto AALC.

Temp (°C)	Langmuir $Q_m$	Parameters B	Freundlich $K_f$	Parameters N
30°C	414.34	0.0662	1.748	2.2700
40°C	419.07	0.0766	1.791	2.3217
50°C	465.63	0.0634	1.758	1.8187
60°C	537.88	0.0931	1.833	2.2802

iron (II) ions within 30 mins of adsorption, hence for effective adsorption of iron (II) ions in aqueous solution using *Averva lanata*.

#### Effect of pH on the batch adsorption of Iron (II) Ions in Aqueous Solution

Effect of pH on adsorption of heavy metals: The pH of the wastewater is one of the imperative factors governing the adsorption of the metal ions. The effect of pH was studied from a range of 2 to 6 under the precise conditions (at optimum contact time of 60 min, 200 rpm shaking speed, with 25 mg of the adsorbents used, and at a room temperature of 30 °C). From Fig. 3, with activated carbon from *Averva lanata* used as adsorbent, it was observed that with increase in the pH (2-6.5) of the wastewater, the percentage removal of iron ((II)) ions increased up to the pH 6.5 as shown above. At pH 6.5, maximum removal was obtained for metal ions, with high % removal of Fe (II). The increase in percentage removal of the metal ions may be explained by the fact that at higher pH the adsorbent surface is deprotonated and negatively charge; hence attraction between the positively metal cations occurred (Shrivastava 2001).

#### Adsorption models

The adsorption equilibrium data were further analyzed into two well known isotherm models via Freundlich and Langmuir models.

#### Freundlich model

The Freundlich model (Namasivayam 2004) which is an indicative of surface heterogeneity of the adsorbent is described by the following equation.

$$\log q_e = \log k_f + 1/n + \log C_e \quad (9)$$

Where  $K_f$  and  $1/n$  are Freundlich constants associated with adsorption capacity and adsorption intensity respectively, The Freundlich plots between  $\log q_e$  and  $\log C_e$  for the adsorption of Fe (II) were drawn. It was found that correlation efficient values were less than 0.99 at both the temperature studied indicating that Freundlich model (Fig. 4) was not applicable to the present study (Table 2).

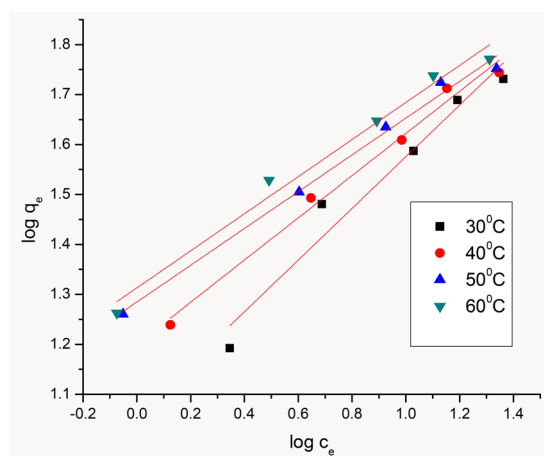


Fig. 4. Freundlich adsorption isotherm for the removal of Fe (II) ion.

### Langmuir model

The adsorption isotherm was also fitted to Langmuir model. The Langmuir equation which is valid for monolayer adsorption (Sharma 2005) on to a surface is given below.

$$1/q_e = 1/q_m + 1/q_{mb} C_e \quad (10)$$

Where  $q_e$  ( $\text{mgg}^{-1}$ ) is the amount adsorbed at the equilibrium concentration  $C_e$  ( $\text{mol L}^{-1}$ ),  $q_m$  ( $\text{mgg}^{-1}$ ) is the Langmuir constant representing the maximum monolayer adsorption capacity and  $b$  ( $\text{L mol}^{-1}$ ) is the Langmuir constant related to energy of adsorption. The plots  $1/q_e$  as a function of  $1/C_e$  for the adsorption of Fe (II) was found linear (Fig. 5). Suggesting the applicability of Langmuir model in the present adsorption system. The correlation coefficient ( $R^2$  near 1) confirm good agreement between both theoretical models and our experimental results the values of the monolayer capacity ( $q_m$ ) and equilibrium constant ( $b$ ) have been evaluated from the intercept and slope of these plots and given in Table 2. It is adsorbent for the Fe (II) is comparable to the maximum adsorption obtained from the adsorption isotherms. These facts suggest that Fe (II) is adsorbed in the form of monolayer coverage on the surface of the prepared adsorbent. Satisfactory fitting of the Langmuir model to the adsorption of Fe (II) on Activated *Averva lanata* adsorbent.

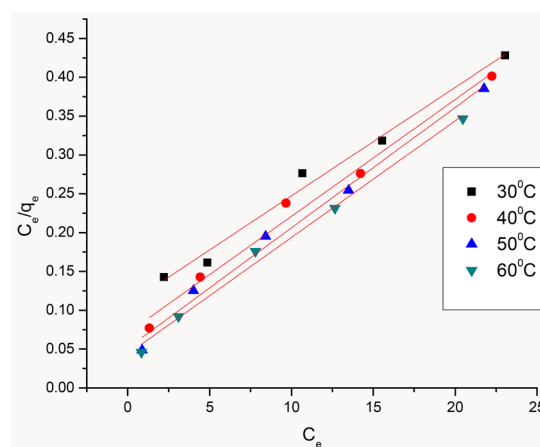


Fig. 5. Langmuir adsorption isotherm for the removal of Fe (II) ion.

### Kinetics study

The Kinetic adsorption data were evaluated to understand the dynamics of the adsorption reaction in terms of the order of the rate constant batch experiments were conducted to explore the rate of Fe (II) adsorption by *Averva lanata* as described in adsorption isotherms section at pH 6.5. Three Kinetic models were applied to the adsorption Kinetic data in order to investigate the behavior of adsorption process (Singh 2001) of Fe (II) onto the adsorbents. These models include the pseudo first order Kinetics (reversible or irreversible), the pseudo – Second – order and the intra particle diffusion models the linear form of reversible pseudo – first – order model can be formulated as:

$$\ln (q_e - q_t) = \ln q_e - k_1 \times t \quad (7)$$

Where  $q_e$  ( $\text{mol/g}$ ) and  $q_t$  ( $\text{mole/g}$ ) are the amount of Fe (II) adsorbed at equilibrium and at time  $t$ , respectively and  $K_1$  ( $\text{min}^{-1}$ ) is the rate constant  $K_1$  values were evaluated from the linear regression of  $\ln (q_e - q_t)$  versus data. Linear form of irreversible pseudo first order model can be formulated as:

$$\ln (C_o/C_t) = K \times t \quad (8)$$

Where  $C_o$  ( $\text{mg/l}$ ) is the initial concentration of Fe (II) and  $C_t$  ( $\text{mg/l}$ ) is equilibrium concentration of Fe (II) at time ' $t$ ' respectively, and  $K$   $\text{min}^{-1}$  is the rate constant

evaluation of data has been done using linear plot of  $\ln(C_o/C_t)$  versus time. The Linear form of pseudo – second – order equation can be formulated as.

$$t/q_t = 1/K_2 q_e^2 + t/q_e \quad (9)$$

Where  $q_e$  and  $q_t$  are surface loading of Fe (II) at equilibrium and time 't' respectively and  $K_2$  (g/mg/min) is the second – order rate constant, The Linear plot of  $t/q_t$  as a function of provided not only the rate constant  $K_2$ , but also an independent evaluation of  $q_e$ . The fitting of experimental data to the pseudo – first – order and the pseudo – second- order equation seemed to be quite good for where the calculated correlation coefficients ( $R^2$ ) almost the same values (Jambulingam 2005).

The Elovich model equation is generally expressed as

$$d_{qt} / d_t = \alpha \exp(-\beta qt) \dots\dots\dots(10)$$

Where;  $\alpha$  is the initial adsorption rate ( $\text{mg g}^{-1} \text{min}^{-1}$ ) and  $\beta$  is the desorption constant (g/mg) during any one experiment. To simplify the Elovich equation, assumed  $\alpha\beta t \gg t$  and by applying boundary conditions  $qt = 0$  at  $t=0$  and  $qt = qt$  at  $t = t$  Eq (10) becomes:

$$q_t = 1/\beta \ln(\alpha\beta) + 1/\beta \ln t \dots\dots\dots(11)$$

If Fe (II) ions adsorption fits with the Elovich model, a plot of  $qt$  vs  $\ln(t)$  should yield a linear relationship with a slope of  $(1/\beta)$  and an intercept of  $(1/\beta) \ln(\alpha\beta)$ . The Elovich model parameters  $\alpha$ ,  $\beta$ , and correlation coefficient ( $\gamma$ ) are summarized in Table 3. The experimental data such as the initial adsorption rate ( $\gamma$ ) adsorption constant ( $\beta$ ) and the correlation coefficient ( $\gamma$ ) calculated from this model indicates that the initial adsorption ( $\alpha$ ) increases with temperature similar to that of initial adsorption rate (h) in pseudo-second-order kinetics models (Ngah 2002). This may be due to increase the pore or active site on the AALC adsorbent.

For adsorption of Fe (II) on to *Averva lanata* the obtained results represent more conformity to pseudo-second order model ( $R^2 = 0.99$ ), the initial adsorption rate  $K_2 q_e^2$  for *Averva lanata*. Kinetic data for the adsorption of Fe (II) were also analyzed ac-

**Table 3.** The Rmodynamic Parameter for the Adsorption of Iron (II) ion onto ALAC.

(C°)	$\Delta G^\circ$				$H\Delta^\circ$	$S\Delta^\circ$
	30°C	40°C	50°C	60°C		
25	-5786.1	-6346.5	-6702.7	-6972.1	6.11	39.51
50	-4319.1	-4798.5	-5878.6	-6068.4	14.96	63.61
75	-3485.4	-3821.6	-4392.9	-4953.7	11.56	49.47
100	-2250.9	-2459.8	-5293.1	-3194.0	15.58	59.39
125	-1289.8	-1613.2	-3613.3	-2199.3	13.52	49.38

ording to intra-particle diffusion model achieve can be formulated as.

$$Qt = K_{qt} 0.5 \quad (12)$$

Where  $qt$  is the amount of Fe (II) adsorbed (mg/g) at time  $t$ , and  $kp$  ( $\text{mg/g min}^{0.5}$ ) is the rate constant for intra – particle diffusion. Results are shown in Table 4. Usually the plot of  $qt$  versus  $t^{0.5}$  may be distinguished in two or more steps taking place during adsorption process including instantaneous adsorption stage by external mass transfer (first sharper portion), intra-particle diffusion which is the rate controlling stage (second portion as the gradual adsorption stage) and the final equilibration of age where the intra – particle diffusion starts to slow down due to extremely low solute concentration in solution (the third portion).

### Adsorption thermodynamics

The thermodynamic parameters (Chien 1980) for the adsorption of Fe (II) ions by Activated *Averva lanata* were determined using the following equations:

$$K_D = qe/C_e \quad (13)$$

$$\Delta G^\circ = -RT \ln K_D \quad (14)$$

$$\ln K_D = (\Delta S^\circ/R) - (\Delta H^\circ/RT) \quad (15)$$

Where  $K_D$  is the distribution coefficient for the adsorption in g/L,  $\Delta G^\circ$  is the Gibbs free energy in J/mol,

$R$  is the universal gas constant in J/mol K,  $T$  is the absolute temperature in K,  $\Delta S^\circ$  is the entropy change in J/mol K and  $\Delta H^\circ$  is the enthalpy change in kJ/mol. The values of Gibbs free energy ( $\Delta G^\circ$ ) for various temperatures were calculated from the experimental

**Table 4.** The kinetic parameters for the adsorption of Iron (II) Ion onto AALC,

C <sub>0</sub>	Temp °C	Pseudo second order			h	Elovich model			Intraparticle diffusion		
		q <sub>e</sub>	K <sub>2</sub>	γ		α	β	γ	K <sub>id</sub>	γ	C
25	30	99.490	0.0018	0.994	19.52	818.20	0.0916	0.9959	1.7335	0.9981	0.1291
	40	100.17	0.0016	0.991	20.90	1203.6	0.0951	0.9968	1.7504	0.9975	0.1225
	50	100.73	0.0014	0.992	20.87	1901.9	0.1004	0.9982	1.7651	0.9969	0.1145
50	60	100.07	0.0014	0.991	22.10	2783.7	0.1052	0.9948	1.7738	0.9973	0.1092
	30	190.41	0.0021	0.992	34.85	1260.1	0.0468	0.9961	1.7045	0.9989	0.1329
	40	192.37	0.0020	0.991	35.97	1460.5	0.0471	0.9987	1.7145	0.9928	0.1302
75	50	195.86	0.0018	0.993	38.53	1968.7	0.0478	0.9967	1.7332	0.9941	0.1251
	60	197.17	0.0017	0.991	40.57	2144.5	0.0477	0.9989	1.7400	0.9948	0.1242
	30	266.65	0.0022	0.992	51.10	2109.2	0.0341	0.9959	1.6825	0.9952	0.1296
100	40	273.50	0.0022	0.994	52.60	2279.9	0.0334	0.9984	1.6953	0.9983	0.1286
	50	280.24	0.0021	0.991	55.94	2501.0	0.0328	0.9967	1.7095	0.9960	0.1276
	60	282.68	0.0020	0.992	47.44	4605.9	0.0362	0.9983	1.7245	0.9940	0.1143
125	30	329.80	0.0024	0.994	54.09	1150.9	0.0248	0.9943	1.6127	0.9946	0.1472
	40	338.49	0.0024	0.995	56.28	1394.5	0.0248	0.9982	1.6317	0.9988	0.1429
	50	343.90	0.0011	0.997	59.50	1673.6	0.0249	0.9972	1.6468	0.9954	0.1393
125	60	351.13	0.0023	0.999	66.09	2414.7	0.0254	0.9969	1.6716	0.9990	0.1324
	30	385.32	0.0022	0.998	57.66	839.01	0.0199	0.9981	1.5570	0.9987	0.1600
	40	392.62	0.0025	0.997	61.02	1034.8	0.0201	0.9948	1.5764	0.9967	0.1545
125	50	405.44	0.0016	0.998	58.86	843.37	0.0188	0.9994	1.5756	0.9961	0.1609
	60	410.50	0.0025	0.992	65.92	1286.2	0.0197	0.9972	1.6052	0.9952	0.1499

data. The values of enthalpy change ( $\Delta H^\circ$ ) and entropy change ( $\Delta S^\circ$ ) were estimated from the slope and intercept of the plot of  $\ln KD$  Vs  $1/T$ . The estimated thermodynamic parameters were tabulated and shown in Table 3. But the negative values of Gibbs free energy change ( $\Delta G^\circ$ ) obtained for the adsorption of Fe (II) ions by Activated *Averva lanata* at various temperatures had shown the spontaneous nature of the adsorption process.

The positive values of enthalpy change ( $\Delta H^\circ$ ) obtained for the adsorption of Fe (II) ions by Activated *Averva lanata* at various temperatures indicated that the adsorption reactions were endothermic. The positive values of entropy change ( $\Delta S^\circ$ ) for the adsorption of Fe (II) ions by Activated *Averva lanata* at various temperatures showed the increased randomness at solid liquid interphase during the sorption processes of Fe (II) ions on the adsorbent AALC. This is a direct consequence of (i) opening up of structure of adsorbent beads (ii) enhancing the mobility and extent of penetration within the adsorbent beads and (iii) overcoming the activation energy barrier and enhancing the rate of intra-particle diffusion

The adsorption of Fe (II) ions by Activated *Aver-*

*va lanata* slightly increased when temperature was raised up to 60 °C. It might be due to the generation of new active sites on the adsorbent surface and also due to the increased rate of pore diffusion. But when the temperature was further raised, adsorption processes had decreased largely. It showed that the adsorption processes of Fe (II) ions by Activated *Averva lanata* were exothermic reactions and physical in nature which involved the weak forces of attraction between the sorbate-sorbent molecules.

## CONCLUSION

Adsorption of iron (II) ions from aqueous solution using activated carbon from waste *Averva lanata* has been investigated. The amount of iron (II) ions adsorbed was found to vary significantly with process parameters such as carbon dosage, initial concentration of adsorbate and contact time. The adsorption process follows Langmuir and Freundlich isotherms but a better sorption fit using Langmuir isotherm model was obtained indicating a monolayer formation over a surface of the material. The monolayer saturation capacity of 537.88 mg of iron (II) ions adsorbed per g of *Averva lanata* activated carbon was obtained and found to be higher than monolayer



saturation capacity of other adsorbent used for iron (II) ions adsorption. Adsorption kinetics was modeled using the pseudo first order, pseudo second order kinetic equations, and intra-particle diffusion models. Sorption kinetics showed good agreement of the experimental data the pseudo second order kinetic reaction is the rate controlling step with some intra particle diffusion taking place.

The high adsorption intensity of *Averva lanata* activated carbon and its affinity for Iron (II) ions can help solve many adsorption challenges in the industry and in water purification processes.

## REFERENCES

- Ahmedna M, Marshall WE, Hussein AA, Rao RM, Goktepel (2004) The use of nutshell carbons in drinking water filters for removal of trace metals. *Water Res* 38: 1062-1068.
- Aziz HA, Yusoff MS, Adlan MN, Adnan NH, Alias S (2004) Physico-chemical removal of iron from semiaerobic landfill leachate by limestone filter. *Water Manag* 24: 353-358.
- Balintova M, Petrlikova A (2010) Study of pH influence on selective precipitation of heavy metals from acid mine drainage. In 14<sup>th</sup> Conference on Environmental and Mineral Processing, VSB-TU, Ostrava, Czech, Republic, pp 160-166.
- Berbenni P, Pollice A, Canziani R, Stabile L, Nobili F (2000) Removal of iron and manganese from hydrocarbon-contaminated groundwaters. *Bioresour Technol* 74: 109-114.
- Bin Jusoh A, Cheng WH, Low WM, Nora'aini A, Noor MJMM (2005) Study on the removal of iron and manganese in groundwater by granular activated carbon. *Desalination* 182: 347-353.
- Chapman D (1992) Water quality assessments: A guide to the use of biota, sediments and water in environmental monitoring. Kluwer Academic Publishers, Dordrecht, pp 372.
- Chien SH, Clayton WR (1980) Application of Elovich Equation to the kinetics of Phosphate release and sorption on soil. *Soil Sci Soc Am J*. 44 :265 – 268.
- Ellis D, Bouchard C, Lantagne G (2000) Removal of iron and manganese from groundwater by oxidation and microfiltration. *Desalination* 130: 255-264.
- El-Sherif IY, Fathy NA (2011) Equilibrium and kinetic study of Cd (II) and Ni (II) ions removal by semi-carbonized/H<sub>3</sub>PO<sub>4</sub> cotton stalks. *EJEAFChe* 10: 2744-2758.
- Girgis BS, Attia AA, Fathy NA (2007) Modification in adsorption characteristics of activated carbon produced by H<sub>3</sub>PO<sub>4</sub> under flowing gases. *Colloids and Surfaces A: Physicochem. Eng Aspects* 299: 79-87.
- Hamadi NK, Swaminathan S, Chen XD (2004) Adsorption of paraquat dichloride from aqueous solution by activated carbon derived from used tires. *J Hazardous Materials* 112 (1-2): 133-141.
- Jambulingam M, Rehugadevi N, Karthikeyan S, Kiruthika J, Patabhi S (2005) Adsorption of Cr (VI) from aqueous solution using a low cost activated carbon. *Ind J Environ Protect* 25(5): 458-463.
- Kazemipour M, Ansari M, Tajrobehkar S, Majdzadeh M, Kermani HR (2008) Removal of lead, cadmium, zinc, and copper from industrial wastewater by carbon developed from walnut, hazelnut, almond, pistachio shell, and apricot stone. *J Hazardous Materials* 150: 322-327.
- Letterman RD (1999) American Water Works Association: Water Quality and Treatment. 5<sup>th</sup> (ed). McGraw- Hill, New York.
- Munter R, Ojaste H, Sutt J (2005) Complexed iron removal from groundwater. *J Environ Eng* 131: 1014-1020.
- Namasivayam C, Holl WH (2004) Chromium (III) removal in tannery wastewaters using Chinese reed (*Miscanthus Sinesis*), a fast growing plant. *Holz Roh Werkst* 62: 74 – 80.
- Ngah WSW, Endud CS, Mayanar R (2002) Removal of copper (II) ions from aqueous solution onto chitosan and cross-linked chitosan beads *React. Funct. Polym.* 50, 181-190.
- Okoniewska E, Lach J, Kacprzak M, Neczaj E (2007) The removal of manganese, iron and ammonium nitrogen on impregnated activated carbon. *Desalination* 206: 251-258.
- Sharma A. Bhattacharya D (2005) Utilisation of biosorbent based on *Azadirachta indica* (Neem) leaves for removal of water soluble Metals. *Ind J Environ Chem.* 12: 285-295.
- Shrivastava RK, Ayachi AK, Mora M (2001) Removal of Cr (VI) by utilization of Bidi leaves. *Pollut Res* 20 (4): 639 – 643.
- Singh IB, Singh DR (2001) Hexavalent chromium removal using iron bearing industrial sludges. *Ind J Chem Tech nol* 8: 487-495.
- Vaaramaa K, Lehto J (2003) Removal of metals and anions from drinking water by ion exchange. *Desalination.* 155: 157-170.